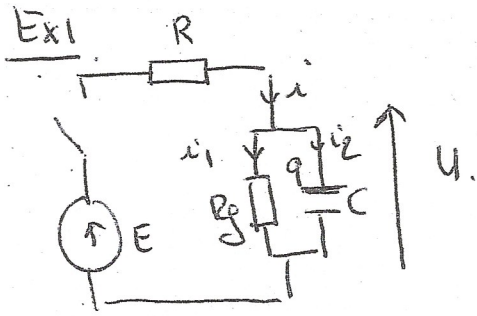


Conexion D1,



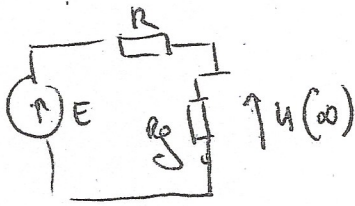
1°] $t=0^-$ (avant fermeture de K), le condensateur est déchargé $\Rightarrow q=0$ et $u = \frac{q}{C}$ donc

$$u(0^-) = 0$$

Par continuité de la tension aux bornes du condensateur.

Sauf que $u(0^+) = 0$.

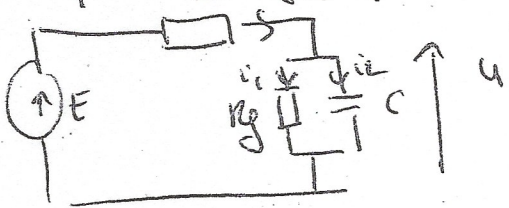
2°] $t \rightarrow \infty$ $i_2(\infty) = 0$, le circuit équivalent est donc le diviseur de tension obtenu.



$$u(\infty) = \frac{R_g}{R + R_g} \cdot E \quad \text{si } R_g \gg R \quad R_g + R \rightarrow R_g$$

et $u(\infty) \rightarrow E$

3°] eq. diff. recherchée pour $u(t)$



$$\begin{cases} E = R i + u & (1) \\ i = i_1 + i_2 & (2) \\ u = R_g i_1 & (3) \\ i_2 = C \frac{du}{dt} & (4) \end{cases}$$

d'où (1) donne $E = R \left[\frac{u}{R_g} + C \frac{du}{dt} \right] + u = \left(\frac{R}{R_g} + 1 \right) u + RC \frac{du}{dt}$

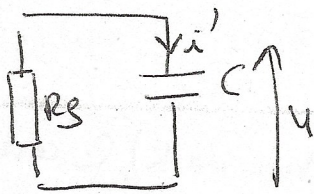
$$E = \frac{R + R_g}{R_g} u + RC \frac{du}{dt} \Rightarrow \frac{du}{dt} + \frac{R + R_g}{R \cdot R_g \cdot C} u = \frac{E}{RC}$$

avec $Z = \frac{R \cdot R_g \cdot C}{R + R_g}$

$$u(t) = A e^{-\frac{t}{Z}} + S_p \quad \text{avec} \quad S_p \cdot \frac{R}{Z} = \frac{E}{RC} \Rightarrow \boxed{S_p = \frac{R_g}{R + R_g} \cdot E} \quad (\text{on retrouve } u(\infty)!)$$

à $t=0^+$ $u(0^+) = 0 \Rightarrow \boxed{u(t) = \frac{R_g \cdot E}{R + R_g} \left(1 - \exp\left(-\frac{t}{Z}\right) \right)}$

4°) On ouvre K, (nouvelle origine des temps), le condensateur se décharge à travers R_g .



$$a \text{ à } b = 0^+ \quad u(0^+) = \frac{R_g \cdot E}{R + R_g}$$

$$i' = C \frac{du}{dt} \text{ et } u = -R_g i' \Rightarrow u = -R_g C \frac{du}{dt} \Rightarrow \boxed{\frac{du}{dt} + \frac{u}{R_g C} = 0}$$

$$z' = R_g C \quad \begin{cases} u(t) = A e^{-\frac{t}{z'}} \\ u(0^+) = \frac{R_g \cdot E}{R + R_g} \end{cases}$$

$$\Rightarrow \boxed{u(t) = \frac{R_g \cdot E}{R + R_g} e^{-\frac{t}{z'}}$$

So) $t_1 = 100 \mu s \quad u = u_1 = 10V$

$$u_1 = \frac{R_g \cdot E}{R + R_g} e^{-\frac{t_1}{z'}} \rightarrow \text{on dit}$$

$$u_1 \approx E e^{-\frac{t_1}{z'}} \text{ en considérant } R_g \gg R$$

$$\rightarrow \frac{u_1}{E} = e^{-\frac{t_1}{z'}} \rightarrow \ln \frac{u_1}{E} = -\frac{t_1}{z'} \Rightarrow z' = -\frac{t_1}{\ln \frac{u_1}{E}} \Rightarrow \boxed{R_g = \frac{t_1}{C \ln \frac{E}{u_1}}}$$

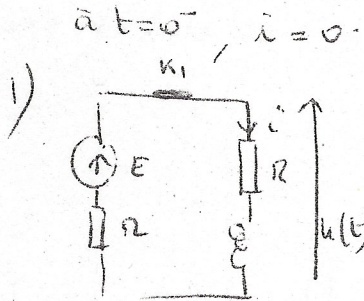
AN $C = 1 \mu F = 10^{-6} F$; $t_1 = 100 \mu s \rightarrow$
 $E = 15V$
 $u_1 = 10V$

$$\boxed{R_g = 250 \Omega}$$

d'où $u = u_2 = 1V \quad t_2 = R_g \cdot C \ln \frac{E}{u_2} = 250 \cdot 10^{-6} \cdot \ln 15 = 677 \mu s = 11 \text{ min}$

Ex Etinelle de rupture.

Partie A



$\text{à } t=0$ K_1 est fermé, K_2 ouvert.

2) $i(t=0^+) = i(t=0^-)$ par continuité du courant de bobine.
- loi des mailles

$$E \pm Ri + u(t) \quad \forall t$$

$$t=0^+ \quad E = 0 + u(t=0^+) \Rightarrow \boxed{u(t=0^+) = E}$$

3) En régime permanent, la bobine se conduit comme un

$$\Rightarrow i(t \rightarrow \infty) = \frac{E}{R+r} \quad (\text{loi de Pédalle})$$

$$u(\infty) = Ri + u_L = \boxed{\frac{R}{R+r} \cdot E = u(\infty)}$$

4) $E = (R+r)i + L \frac{di}{dt} \Rightarrow \frac{di}{dt} + \frac{i}{\tau} = \frac{E}{L}$ $\tau = \frac{L}{R+r}$

$$i(t) = Ae^{-\frac{t}{\tau}} + \frac{E}{R+r} \Rightarrow i(t) = \frac{E}{R+r} + Ae^{-\frac{t}{\tau}}$$

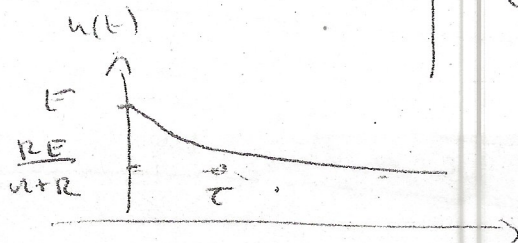
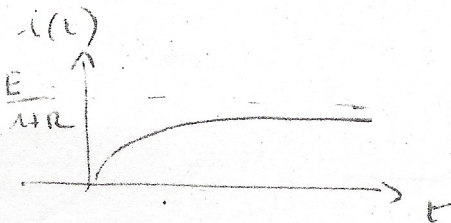
$$t \geq 0^+ \quad i=0 \Rightarrow A = -\frac{E}{R+r}$$

$$\boxed{i(t) = \frac{E}{R+r} \left[1 - e^{-\frac{t}{\tau}} \right]}$$

$$u(t) = L \frac{di}{dt} + Ri = \frac{LE}{R+r} e^{-\frac{t}{\tau}} + \frac{RE}{R+r} \left(1 - e^{-\frac{t}{\tau}} \right)$$

$$u(t) = \frac{R \cdot E}{R+r} + E \left(1 - \frac{R}{R+r} \right) e^{-\frac{t}{\tau}}$$

$$\Rightarrow \boxed{u(t) = \frac{R \cdot E}{R+r} + \frac{E \cdot r}{R+r} e^{-\frac{t}{\tau}}}$$



cohérent car τ
 S_p correspond à
régime forcé.